

1 **High-resolution velocity estimation from surface-based** 2 **common-offset GPR reflection data**

3
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7 8 **Summary**

9 Surface-based common-offset ground-penetrating radar (GPR) reflection profiling is a popular
10 geophysical exploration technique for obtaining high-resolution images of the shallow
11 subsurface in a cost-effective manner. One drawback of this technique is that, without
12 complementary borehole information in form of dielectric permittivity and/or porosity logs
13 along the profile, it is currently not possible to obtain reliable estimates of the high-frequency
14 electromagnetic velocity distribution of the probed subsurface region. This is problematic
15 because adequate knowledge of the velocity is needed for accurate imaging and depth
16 conversion of the data, as well as for quantifying the distribution of soil water content. To
17 overcome this issue, we have developed a novel methodology for estimating the detailed
18 subsurface velocity structure from common-offset GPR reflection measurements, which does
19 not require additional conditioning information. The proposed approach combines two key
20 components: Diffraction analysis is used to infer the smooth, large-scale component of the
21 velocity distribution, whereas the superimposed small-scale fluctuations are inferred via
22 inversion of the reflected wavefield. We test and validate our method on two synthetic datasets

23 having increasing degrees of complexity and realism before applying it to a field example from
24 the Boise Hydrogeophysical Research Site (BHRS), where independent control data in the
25 form of neutron-neutron porosity logs are available for validation. The results obtained
26 demonstrate the viability and robustness of the proposed approach. Further, due to its efficiency,
27 both in terms of field effort and computational cost, the method can be readily extended to 3D,
28 which further enhances its attractiveness compared to multi-offset-based GPR velocity
29 estimation techniques.

30

31 **Abbreviated title:** Velocity estimation from common-offset GPR data

32

33 **Keywords:** Electrical properties; Hydrogeophysics; Electromagnetic theory; Ground
34 penetrating radar; Inverse theory; Wave scattering and diffraction.

35

36 **1 Introduction**

37 Ground-penetrating radar (GPR) is a high-resolution geophysical exploration technique that
38 has the potential of providing images of shallow subsurface structure with a resolution in the
39 meter to decimeter range (e.g., Knight 2001; Annan 2005; Klotzsche et al. 2018; Lai et al.,
40 2018). Whereas borehole-based GPR transmission techniques have proven to be well-suited to
41 full-waveform inversion approaches (e.g., Ernst et al. 2007; Klotzsche et al. 2019), estimating
42 the detailed velocity structure of the subsurface from surface-based GPR reflection data is
43 notoriously difficult. This is problematic because: (i) the overwhelming majority of GPR data
44 are acquired in reflection mode along the Earth's surface; (ii) accurate velocity information is

45 necessary for proper imaging of reflection data; and (iii) the high-frequency electromagnetic
46 wave velocity in the GPR regime has a strong and direct sensitivity to soil water content, which
47 is a key parameter for many hydrogeological, agricultural, and engineering applications (e.g.,
48 Huisman et al. 2003).

49

50 One common approach for subsurface velocity estimation from reflection GPR measurements
51 is to collect data at multiple transmitter-receiver offsets and to perform either normal-moveout
52 (NMO) velocity analysis (e.g., Greaves et al. 1996; Huisman et al. 2003; Perroud & Tygel 2005)
53 or reflection tomography (e.g., Bradford 2008). With regard to NMO, the inherent assumption
54 of 1D horizontal layering means that it cannot effectively deal with the highly heterogeneous
55 velocity structures that are rather common in near-surface investigations. Although reflection
56 tomography is able to overcome this issue, it comes at a rather high computational cost and
57 requires inherently subjective horizon picking. Further, as pointed out by Bradford et al. (2009),
58 reflection tomography only recovers the large-scale component of the subsurface velocity
59 distribution that is needed to properly focus and image the GPR data, which is of substantially
60 lower resolution than the reflection image itself. The latter problem can be potentially
61 alleviated through waveform inversion approaches (e.g., Busch et al. 2012; Lavoué et al. 2014);
62 however their success so far has been limited due to the rather narrow range of reflection angles
63 and antenna radiation patterns that are highly complex, largely unknown, and site-dependent
64 (e.g., Lampe & Holliger 2003). Finally, a clear drawback of multi-offset GPR acquisitions is
65 their high cost in terms of acquisition time, which increases approximately linearly with the
66 considered number of transmitter-receiver offsets for the common case of GPR systems having

67 a single transmitter and receiver antenna. Indeed, such surveys become largely impractical in
68 the context of long 2D profiles and, particularly, 3D acquisitions.

69

70 For the above reasons, the vast majority of surface-based GPR reflection surveys are performed
71 using the traditional bi-static, common-offset approach, where a single transmitter-receiver
72 antenna pair, separated by a small fixed distance, is incrementally moved along the
73 measurement profile (e.g., Annan 2005). While the estimation of the subsurface velocity
74 distribution from such data is substantially more difficult than for multi-offset GPR surveys,
75 significant efforts have been made during the past decade because of the high potential rewards.

76 In this regard, Schmelzbach et al. (2012) present an impedance inversion approach for
77 common-offset GPR data that is based on a convolution model for the GPR traces, where
78 borehole dielectric permittivity or porosity logs are used to recover the low-frequency part of
79 the velocity structure that cannot be obtained from the reflection data. Zeng et al. (2015) and
80 Liu et al. (2018) adopt similar approaches to estimate the distribution of soil water content and
81 to characterize buried archaeological remains, respectively. Xu et al. (2021) also assume a
82 convolution model for the GPR traces, but combine stochastic simulation with simulated
83 annealing optimization in order to generate velocity realizations that honor the GPR
84 measurements and borehole porosity log data along the profile. Forte et al. (2013; 2014) assume
85 a locally 1D layered subsurface structure and use picked reflection amplitudes to recursively
86 estimate the GPR velocity in a series of identified subsurface layers, in which the velocity is
87 assumed constant. Other authors estimate the spatial distribution of GPR velocity from
88 common-offset data via the analysis of diffractions present in the recordings. Novais et al.

89 (2008) use velocity continuation to generate several migrated sections and analyze the
90 associated diffraction focusing to build a root-mean-square (RMS) velocity model. Clair &
91 Holbrook (2017) apply the seismic diffraction imaging and velocity analysis workflow
92 proposed by Fomel et al. (2007) to common-offset GPR data in order to estimate snow water
93 equivalent. Yuan et al. (2019) employ a similar approach to characterize the velocity structure
94 of surficial chalk deposits. Although all of the above methods have the ability to estimate
95 subsurface properties from common-offset GPR measurements, they all suffer from inherent
96 limitations. Notably, the reflection-based methods have the potential to provide high-resolution
97 results, but they generally require complementary information such as borehole logs, which are
98 usually not available. Conversely, diffraction-based methods require a suitably dense and even
99 distribution of diffractions in the data and, even under ideal circumstances, can only resolve
100 the large-scale velocity structure.

101

102 In this study, we present a novel velocity estimation method for surface-based common-offset
103 GPR reflection data that combines the advantages of the reflection- and diffraction-based
104 techniques described above. To estimate the low-frequency background velocity field,
105 diffractions are separated from the unmigrated GPR data and subjected to migration velocity
106 analysis based on a prescribed focusing measure. After migrating the GPR data using the
107 derived velocity field, the reflected wavefield is isolated and used to deduce the small-scale
108 velocity fluctuations. The latter is accomplished via sparse inversion based on an iteratively
109 reweighted least-squares strategy assuming a convolutional model for each GPR trace. The
110 final high-resolution velocity distribution is obtained by combining the large-scale diffraction-

111 based and the fine-scale reflection-based estimates.

112

113 The paper proceeds as follows. We begin by describing the methodological background of the
114 proposed velocity estimation method. Next, we show the application of our method to two
115 synthetic datasets, which differ in their degree of complexity and realism. Finally, we apply the
116 proposed approach to common-offset 100-MHz GPR field data acquired at the Boise
117 Hydrogeophysical Research Site (BHRS) near Boise, Idaho, USA.

118

119 **2 Methodology**

120 We assume in our work that the subsurface velocity distribution $v(x, z)$ can be regarded as
121 the sum of a smoothly varying or constant background velocity field $v_0(x, z)$ and a small-
122 scale velocity fluctuation field $\Delta v(x, z)$ (e.g., Pullammanappallil et al. 1997; Poppeliers 2007;
123 Irving et al. 2009; Scholer et al. 2010)

$$v(x, z) = v_0(x, z) + \Delta v(x, z). \quad (1)$$

124 To determine $v(x, z)$ from a common-offset GPR reflection dataset, we separate the recorded
125 wavefield into its diffracted and reflected components, which are used to estimate v_0 and Δv ,
126 respectively. This inherently assumes that the background velocity field is smooth at the scale
127 of a dominant GPR wavelength and beyond, such that it does not contribute to the reflected
128 wavefield. Figure 1 illustrates schematically the steps involved in our velocity estimation
129 procedure. First, diffractions are separated and analyzed in order to infer the spatially variable
130 RMS and interval velocity structures. The latter serves as v_0 , whereas the former is used to
131 migrate the common-offset GPR data, after which the dominant reflections are separated.

132 Assuming a convolutional relationship between the velocity perturbation field and the
133 reflection data based on an estimated mixed-phase wavelet, a L1-norm constrained inversion
134 is then used to infer Δv . Below we describe in detail this inversion workflow in terms of the
135 following four main components: (i) diffraction separation, (ii) background velocity estimation,
136 (iii) reflected wavefield prediction, and (iv) velocity perturbation inversion.

137

138 **2.1 Diffraction separation**

139 The diffracted wavefield is obtained in our methodology via plane-wave destruction (PWD)
140 filtering (Fomel, 2002). The underlying assumption when using this approach is that reflections
141 correspond primarily to coherent events having slowly changing slopes in the x - t domain,
142 whereas the slopes associated with diffractions are significantly more spatially variable. The
143 goal of PWD filtering is to destroy locally planar events in the data corresponding to an
144 estimated slope field $\sigma(x, t)$. By regularizing the estimation problem, it is possible to destroy
145 only those events whose slopes change slowly in space, thereby isolating the diffracted energy.

146

147 A local plane wave in the x - t domain can be expressed by the following differential equation
148 (e.g., Fomel, 2002):

$$\frac{\partial u}{\partial x} + \sigma \frac{\partial u}{\partial t} = 0, \quad (2)$$

149 where $u(x, t)$ is the wavefield and σ is the local slope. If the local slope in a seismic or GPR
150 dataset is unchanging in time, the wavefields observed at two adjacent trace positions x_i and
151 x_{i+1} are related by a time shift $\sigma \Delta x$, where Δx is the trace spacing. That is,

$$u(x_{i+1}, t) = u(x_i, t + \sigma\Delta x), \quad (3)$$

152 which has the Fourier transform

$$U(x_{i+1}, \omega) = U(x_i, \omega)e^{i\omega\sigma\Delta x}. \quad (4)$$

153 Equation (4) shows that we can predict the trace at position x_{i+1} from the trace at position x_i
 154 by application of a linear phase shift. To apply this concept to data with temporally variable
 155 local slopes, Fomel (2002) used the fractional delay filter of Thiran (1971) to derive a localized,
 156 discrete, time-domain approximation to $e^{i\omega\sigma\Delta x}$ whose coefficients depend nonlinearly on the
 157 local slope values. Prediction of a trace using its neighbor can then be accomplished by matrix-
 158 vector multiplication

$$\mathbf{u}_{i+1} = \mathbf{P}_{i,i+1}\mathbf{u}_i, \quad (5)$$

159 where $\mathbf{P}_{i,i+1}$ is a time-variable convolution matrix linking trace vectors \mathbf{u}_{i+1} and \mathbf{u}_i , whose
 160 entries are a nonlinear function of the local slope field $\sigma(x, t)$.

161

162 The PWD problem seeks to estimate $\sigma(x, t)$ by minimizing the prediction error for an entire
 163 seismic or GPR section, thereby destroying the local plane waves in the data. Considering the
 164 section \mathbf{s} as a column vector containing all of the traces, i.e., $\mathbf{s} = [\mathbf{s}_1^T \mathbf{s}_2^T \dots \mathbf{s}_n^T]^T$, this is
 165 described by

$$\mathbf{r} = \mathbf{D}\mathbf{s}, \quad (6)$$

166 where \mathbf{r} is the destruction residual, and \mathbf{D} is the destructor matrix defined by:

$$\mathbf{D} = \begin{bmatrix} -\mathbf{P}_{1,2} & \mathbf{I} & 0 & \dots & 0 \\ 0 & -\mathbf{P}_{2,3} & \mathbf{I} & \dots & 0 \\ \dots & \dots & \dots & \dots & \dots \\ 0 & \dots & 0 & -\mathbf{P}_{n-1,n} & \mathbf{I} \end{bmatrix}, \quad (7)$$

167 with \mathbf{I} representing identity operator. The estimation of $\sigma(x, t)$ is accomplished via

168 regularized nonlinear least-squares minimization of equation (6), where shaping regularization
 169 (Fomel 2007a) is used to control the smoothness of the estimated slope field. In our case, the
 170 considered lateral smoothing radius for the regularization must be large enough to estimate a
 171 slope field that well represents the reflections in the dataset, but not the diffractions. The
 172 prediction residual corresponding to the estimated slope field is simply the GPR section with
 173 the reflection events removed. All of the above steps are performed in our work using the
 174 programs ‘sfdip’ and ‘sfpwd’ in Madagascar (<https://reproducibility.org/>), an open-source data
 175 analysis package.

176

177 **2.2 Background velocity estimation**

178 Once the diffracted wavefield has been separated, the next step is to use it to estimate the low-
 179 frequency background velocity field v_0 , which, due to its smoothness at the wavelength scale,
 180 does not contribute to the reflected wavefield. To this end, we first estimate the RMS velocity
 181 distribution by examining the focusing of diffractions during migration using a suite of constant
 182 velocity values. Fomel et al. (2007) proposed a migration focusing metric based on local
 183 kurtosis, whereas Decker et al. (2017) considered the local semblance attribute. Here, we use
 184 the latter measure, which can be defined as

$$s(x, t, v) = \frac{\left(F_v(a(x, t)) \right)^2}{F_v(a^2(x, t))}, \quad (8)$$

185 where $a(x, t)$ denotes the diffraction amplitude as a function of horizontal position x and
 186 time t , and operator F_v denotes time migration using constant velocity v . Migration is
 187 performed on both the diffracted wavefield and its square using the velocity continuation

188 method of Fomel (2003), which results in two space-time-velocity cubes. In Madagascar, this
189 step is accomplished using the program ‘sfvelcon’. The division in equation (8) is then
190 performed in a regularized manner using the program 'sfdivn' in order to constrain the
191 smoothness of the resulting local semblance cube (Fomel, 2007b). Using the automatic picking
192 algorithm 'sfpick' (Fomel, 2009), the maxima on each time-velocity panel are next selected,
193 which yields a 1D RMS velocity curve at each trace location. These curves are combined into
194 a 2D RMS velocity model, which is finally provided as input to the constrained Dix inversion
195 program 'sfdix' (Fomel and Guitton, 2006) to estimate $v_0(x, t)$.

196

197 **2.3 Reflection separation**

198 In order to obtain the reflected wavefield that is used in our inversion procedure to estimate the
199 velocity perturbation Δv , two steps are performed. First, the GPR profile is time-migrated
200 based on the inferred RMS velocity model from Section 2.2 using the velocity continuation
201 method described in Fomel (2003). This has the effect of collapsing diffractions and moving
202 dipping reflectors to their correct positions in terms of vertical traveltimes, and is accomplished
203 using the Madagascar programs 'sfvelcon' and 'sfslice'. Then, we apply the PWD method to the
204 migrated reflection section in order to estimate the local slopes, which in this case are used to
205 predict the time-migrated reflected wavefield void of migration artifacts and random noise
206 (Fomel and Guitton, 2006). The latter step is accomplished using the Madagascar program
207 ‘sfpwsmooth2’. Note that our use of PWD here is different compared to what was presented
208 in Section 2.1, where the method was used to suppress reflected energy in the data and isolate
209 the diffracted wavefield. In this regard, it is important to note that a high-quality reflection

210 section cannot be obtained by simply subtracting the diffracted wavefield from the GPR data.
211 Indeed, predicting the reflected wavefield from the estimated slopes of the time-migrated
212 image results in a cleaner section that is much more amenable to the velocity perturbation
213 inversion described next.

214

215 **2.4 Velocity perturbation inversion**

216 To estimate the velocity perturbation field Δv , we perform sparse inversion of the time-
217 migrated reflected GPR wavefield obtained in Section 2.3. To this end, we assume that the
218 wavefield can be effectively described using the so-called primary reflectivity section (PRS)
219 model (e.g., Gibson and Levander, 1990; Holliger et al., 1994; Irving et al., 2009), whereby the
220 time-migrated data, $d(x, t)$, are expressed as the convolution product of the GPR source
221 wavelet, $w(t)$, and the subsurface reflectivity distribution, $r(x, t)$

$$d(x, t) = w(t) * r(x, t). \quad (9)$$

222 Equation (9) is well known to provide an adequate model for zero-offset seismic or GPR
223 reflection data when single scattering prevails and dispersion is absent (e.g., Yilmaz, 2001). P
224 Although the second assumption is only strictly valid for GPR data acquired in perfectly
225 electrically resistive environments, experience has shown that this model is able to
226 accommodate the limited dispersion effects linked to low-loss conditions for which the GPR
227 method is suitable (e.g., Irving et al., 2009; Xu et al., 2020). Indeed, such effects in GPR data
228 tend to be inherently rather minor, as it is simply impossible to acquire high-quality GPR
229 reflection data in strongly dispersive environments.

230

231 As the subsurface reflectivity can be approximated using the temporal derivative of the velocity
 232 perturbation field (e.g., Pullammanappallil et al. 1997; Poppeliers 2007), and because the
 233 temporal derivative operator may be treated as a finite-difference filter whose position within
 234 a convolution equation can be shifted (Irving et al. 2009; Scholer et al. 2010), equation (9)
 235 leads to

$$\begin{aligned} d(x, t) &\approx w(t) * \frac{\partial}{\partial t} \Delta v(x, t) \\ &= g(t) * \Delta v(x, t), \end{aligned} \quad (10)$$

236 where $g(t)$ represents the time-differentiated GPR wavelet. Expression (10) provides a linear
 237 relationship between the time-migrated reflected GPR wavefield and the velocity perturbation
 238 field, which forms the basis for our inversion procedure. Indeed, considering data vector \mathbf{d}
 239 containing all of the GPR traces arranged into a single column, i.e., $\mathbf{d} = [\mathbf{d}_1^T \mathbf{d}_2^T \dots \mathbf{d}_n^T]^T$, and
 240 model vector \mathbf{m} containing the corresponding velocity perturbations underlying each trace
 241 arranged into a single column, i.e., $\mathbf{m} = [\Delta v_1^T \Delta v_2^T \Delta v_3^T \dots \Delta v_n^T]^T$, we have

$$\mathbf{d} = \mathbf{Gm}, \quad (11)$$

242 where \mathbf{G} is a block-diagonal matrix containing n replicates of the convolution matrix
 243 associated with the time-differentiated wavelet $g(t)$.

244

245 To define the kernel matrix \mathbf{G} , information on the GPR source wavelet is required. In this work,
 246 we estimate $w(t)$ from the reflected wavefield using the method of Schmelzbach & Huber
 247 (2015), which assumes that a typical mixed-phase GPR source wavelet can be considered as a
 248 minimum-phase wavelet that has been shifted by a constant phase angle. To first estimate the
 249 corresponding minimum-phase wavelet, we perform standard least-squares spiking
 250 deconvolution on the reflected wavefield and take the inverse of the deconvolution operator

251 (e.g., Buttkus, 2000). A search of the phase rotation angle that maximizes the kurtosis when
 252 applied to this minimum-phase wavelet is then used to obtain the final mixed-phase GPR
 253 source wavelet. The practical validity of this source wavelet estimation procedure was recently
 254 demonstrated by Xu et al. (2021). Note that the effects of minor dispersion in the GPR data are,
 255 at least in part, accounted for in the sense that an effective wavelet that best fits the considered
 256 dataset in its entirety, rather than the true emitted GPR source signal, is estimated.

257

258 To invert for the velocity perturbation \mathbf{m} given the reflection data \mathbf{d} , we minimize the
 259 following objective function

$$\theta(\mathbf{m}) = \|\mathbf{G}\mathbf{m} - \mathbf{d}\|_2^2 + \lambda \|\mathbf{D}\mathbf{m}\|_1, \quad (12)$$

260 where $\|\cdot\|_p$ denotes the L-p norm, λ is a trade-off parameter that controls the desired balance
 261 between fitting the data and honoring the prescribed prior information about the model, and
 262 matrix \mathbf{D} is given by

$$\mathbf{D} = \begin{bmatrix} \mathbf{D}_x \\ \alpha \mathbf{D}_t \end{bmatrix}. \quad (13)$$

263 Here, \mathbf{D}_x and \mathbf{D}_t are finite-difference matrices that approximate the first derivatives of the
 264 velocity perturbation model in the horizontal and temporal directions, respectively, and α is
 265 an anisotropy parameter that controls the degree of desired smoothing between the temporal
 266 and horizontal directions. The choice of α should reflect the expected aspect ratio of the
 267 underlying GPR velocity heterogeneity.

268

269 Equation (12) corresponds to a regularized least-squares inversion with blocky model prior
 270 constraints. That is, in seeking to minimize the L1-norm of the first derivatives of the velocity

271 perturbation field, we tend to recover models that have a sparse first derivative structure,
 272 meaning a piecewise-constant or blocky appearance. Note that this approach has similarities to
 273 sparse spike deconvolution in seismic data processing, which uses sparsity constraints to
 274 recover the underlying reflectivity series from a seismic trace (e.g., Claerbout and Miur, 1973;
 275 Oldenburg et al., 1983; Velis, 2008). Our method differs, however, in the sense that (i) we use
 276 sparsity applied to the first derivative of the velocity perturbation field and invert for the latter
 277 directly, rather than inverting for a sparse reflectivity series; and (ii) we invert all traces at once
 278 with both vertical and lateral regularization constraints in order to estimate the full 2D velocity
 279 perturbation field.

280

281 Due to the presence of the L1-norm, the minimization of equation (12) is nonlinear. To address
 282 this, we use an iteratively reweighted least squares (IRLS) approach based on the following
 283 approximation of the L_p-norm proposed by Ekblom (1973):

$$\|\mathbf{x}\|_p \approx \sum_{i=1}^n (x_i^2 + \epsilon^2)^{p/2}, \quad (14)$$

284 where ϵ is a small user-defined value (e.g., Farquharson and Oldenburg, 1998). Taking the
 285 derivative of equation (12) with respect to \mathbf{m} and setting it to zero, and considering
 286 approximation (14), we arrive at

$$(2\mathbf{G}^T\mathbf{G} + \lambda\mathbf{D}^T\mathbf{R}\mathbf{D}) \mathbf{m} = 2\mathbf{G}^T\mathbf{d}, \quad (15)$$

287 where

$$\mathbf{R}_{ii} = \frac{1}{|(\mathbf{D}\mathbf{m})_i| + \epsilon} \quad (16)$$

288 is a diagonal reweighting matrix. We solve for \mathbf{m} iteratively as follows:

289

- 290 (1) Set $\mathbf{R} = 2\mathbf{I}$.
- 291 (2) Solve equation (15) for \mathbf{m} using the conjugate gradient method.
- 292 (3) Update \mathbf{R} using equation (16) and the result for \mathbf{m} obtained in Step 2.
- 293 (4) Return to Step (2) and iteratively update \mathbf{m} until a defined maximum number of iterations
294 or desired data fit is reached.

295

296 In carrying out the above steps, the first iteration of our inversion procedure solves for the
297 velocity perturbation field corresponding to an L2-norm constraint on the model derivative
298 term in equation (12). This and subsequent solutions are then used within the IRLS reweighting
299 scheme in order to gradually converge to the L1-norm solution, typically within a few iterations.
300 Once $\Delta v(x, t)$ has been obtained, it is added to the estimated background velocity model
301 $v_0(x, t)$ from Section 2.2. As a final step, the resulting subsurface velocity field in terms of
302 vertical two-way traveltime, $v(x, t)$, is converted to depth to obtain the desired $v(x, z)$.

303

304 **3 Results**

305 **3.1 Application to synthetic data**

306 In the following, we test and validate the velocity estimation technique outlined in Section 2
307 and illustrated in Figure 1 by applying it to synthetic common-offset GPR reflection data. We
308 first consider a layered subsurface velocity model containing a small number of well-defined
309 point-type diffractors. We then move to an arguably more realistic scenario involving a
310 stochastic velocity distribution characterized by the explicit absence of idealized diffracting

311 structures.

312

313 3.1.1 Layered model

314 Our layered velocity model, which is shown in Figure 2a, is similar to that recently considered
315 by Yuan et al. (2019) in a diffraction imaging study. The model contains two main velocity
316 units separated by a dipping interface. A thin horizontal bed, with a thickness of 0.5 m, is
317 present in the underlying unit. Both the upper and lower units contain three circular diffractors
318 with diameters ranging from 0.4 to 0.6 m. The corresponding relative dielectric permittivities
319 of the upper and lower layers, the thin bed, and the diffractors are 9, 16, 25, and 4, respectively.
320 The electrical conductivity of all materials is fixed at a constant value of 1 mS/m, and the
321 magnetic permeability is assumed to be equal to its value in free space.

322

323 Synthetic common-offset GPR reflection data were simulated over the layered velocity model
324 using the gprMax software (Warren et al. 2016), which solves Maxwell's equations using the
325 finite-difference time-domain (FDTD) method. The transmitter and receiver antennas, which
326 are approximated by point electric dipoles, were spaced 0.5 m apart and moved at 0.1 m
327 increments along the survey profile. The source antenna current function was specified as a
328 Ricker wavelet having a dominant frequency of 100 MHz, which resulted in a propagating
329 electromagnetic pulse corresponding to the first derivative of this function. The resulting
330 synthetic GPR data were then contaminated with 2% Gaussian random noise (Figure 2b) prior
331 to being subjected to a standard processing flow involving (i) elimination of the direct air and
332 ground arrivals from the data by subtracting the average trace calculated over a time window

333 from 0 to 36 ns using a moving spatial window of 50 traces; (ii) amplitude scaling to
334 compensate for energy spreading, absorption, and scattering using a gain function of the form
335 $g(t) = (1 + at)e^{bt}$; and (iii) 5-300 Hz bandpass filtering. With time measured in nanoseconds,
336 the parameters a and b were chosen empirically to be 0.3 ns^{-1} and 0.2 ns^{-1} , respectively, such
337 that the gain function brought all amplitudes along a given trace to the same average level.
338 Figure 3a shows the resulting unmigrated processed data section.

339

340 Following the velocity estimation workflow outlined in Section 2 and illustrated in Figure 1,
341 diffractions were first separated from the processed data using PWD filtering (Figure 3b). The
342 diffracted wavefield was then subjected to velocity continuation and local kurtosis analysis in
343 order to estimate the RMS velocity structure (Figure 3c), which was used in a Dix inversion
344 procedure to obtain the low-frequency background velocity field displayed in Figure 3d. Note
345 that this result shows some resemblance to the underlying model in Figure 2a. However, it fails
346 to adequately represent the dipping interface as a sharp discontinuity having a constant slope,
347 and it entirely misses the thin bed. In Figure 3e, we show the GPR reflection data after time
348 migration based on the estimated RMS velocity structure in Figure 3c. We see that the data
349 have been adequately imaged apart from some residual “smiles”, which are attenuated through
350 the application of PWD to isolate the specular reflections (Figure 3f). From the separated
351 reflection image, a mixed-phase GPR wavelet was estimated (Schmelzbach & Huber 2015),
352 which is compared with the first derivative of the Ricker source current function in Figure 3g.
353 Figure 3h shows the velocity perturbation field inferred through our L1-norm inversion
354 approach using a value of $\alpha = 10$ and after 5 IRLS iterations. We observe that the high-

355 frequency elements present in Figure 2a have now been estimated, but not the low-frequency
356 velocity trend. Finally, Figures 3i and 3j show the complete estimated velocity model, equal to
357 the sum of the background and perturbation fields, in terms of two-way traveltime and after
358 conversion to depth, respectively. The comparison with the reference velocity model (Figure
359 2a) is quite favorable, which clearly illustrates the potential benefits of the proposed
360 diffraction- and reflection-based velocity estimation approach. In this context, is important to
361 emphasize that the former can only resolve the smooth large-scale velocity structure and, hence,
362 entirely misses the presence of the thin bed (e.g., Yuan et al. 2019) whereas, on its own, the
363 latter requires coincident borehole information for calibration and recovery of the large-scale
364 component of the velocity structure (e.g., Schmelzbach et al. 2012; Xu et al. 2021).

365

366 3.1.2 Heterogeneous model

367 We now test our proposed methodology on an arguably more realistic model of the shallow
368 subsurface. In this regard, we consider the stochastic velocity distribution shown in Figure 4a,
369 which is meant to emulate a heterogeneous surficial alluvial environment. The model was
370 geostatistically generated based on the von Kármán autocorrelation function, which describes
371 a band-limited fractal medium (e.g., Tronicke & Holliger 2005) and is given by

$$C(r) = \frac{r^\nu K_\nu(r)}{2^{\nu-1} \Gamma(\nu)}, \quad (17)$$

372 where $K_\nu(r)$ is the modified Bessel function of the second kind of order $0 \leq \nu \leq 1$, Γ is the
373 gamma function and

$$r = \sqrt{(x/a_x)^2 + (z/a_z)^2} \quad (18)$$

374 is the weighted radial autocorrelation lag with a_x and a_z denoting the correlation lengths

375 along horizontal and vertical directions x and z , respectively. Values of $v = 0.5$, $a_x = 2.0$ m,
376 and $a_z = 0.2$ m were considered, along with a mean velocity of 0.1 m/ns and a standard
377 deviation equal to 0.01 m/ns. The generated multi-Gaussian velocity realization was then
378 transformed into a facies-type distribution through thresholding, whereby six units having
379 constant velocities equal to 0.079, 0.092, 0.100, 0.105, 0.108, and 0.116 m/ns were specified.

380

381 To generate synthetic common-offset GPR reflection data over the velocity model in Figure 4a,
382 we again used the gprMax software (Warren et al. 2016). Velocity values v were converted to
383 relative dielectric permittivity ϵ for the FDTD modeling using the low-loss approximation
384 $v \approx 1/\sqrt{\epsilon\mu}$, where the magnetic permeability μ was assumed equal to its value in free space.

385 As was done previously, the electrical conductivity was fixed at a constant value of 1 mS/m.

386 For the source antenna current function, we considered for this simulation the derivative of a
387 Blackman-Harris window having a dominant frequency of 100 MHz (Irving and Knight, 2006).

388 The spacing between the transmitter receiver antennas was again set to 0.5 m, and traces were
389 simulated every 0.1 m along the profile. Figure 4b shows the resulting synthetic GPR data with
390 the addition of 2% Gaussian noise. Processing of these data was essentially identical to that for
391 the layered synthetic velocity model except that the averaging window used for the first-arrival
392 removal was set from 0 to 25 ns, and the gain parameters a and b were set to 0.2 ns^{-1} and
393 0.2 ns^{-1} , respectively. The processed GPR section is shown in Figure 5a.

394

395 Figure 5b shows the diffracted wavefield estimated from the processed data in Figure 5a, which
396 was used to infer the RMS velocity structure (Figure 5c) and, subsequently, the background

397 velocity field through Dix inversion (Figure 5d). In Figure 5e, we show the time-migrated GPR
398 section based on the RMS velocity field, from which the reflected wavefield was obtained
399 (Figure 5f). The latter was used to estimate an effective mixed-phase source wavelet, which is
400 shown in Figure 5g and seen to compare favorably to the true source wavelet corresponding to
401 the derivative of the considered input current function. Finally, in Figures 5h, 5i, and 5j, we
402 show the inverted velocity perturbation field obtained after 5 IRLS iterations using a value of
403 $\alpha = 10$, along with the final estimated velocity model in terms of two-way traveltimes and depth,
404 respectively. Comparison of Figure 5j with the underlying velocity model in Figure 4a
405 demonstrates remarkably good agreement, but also points to two interesting aspects of the
406 proposed velocity estimation method that did not become evident in its application to the more
407 idealized layered model (Figures 2 and 3). The first concerns the influence of the direct wave
408 and its muting, which, in the presence of small-scale heterogeneity, inherently affects the
409 viability and accuracy of the velocity estimation over a depth range corresponding to
410 approximately one dominant wavelength, that is, the first ~ 1 m depth. The second observation
411 concerns the importance of the background velocity model and its impact on the final result.
412 This is illustrated by the fact that our final velocity model (Figure 5j) misses the pervasive low-
413 velocity zone between ~ 2 and ~ 3.5 m depth in the central and right-hand side of the model
414 from ~ 7 m to ~ 20 m lateral distance, which can be directly related to the limited resolution of
415 the estimated background velocity model.

416

417 **3.2 Application to field data**

418 3.2.1 Database

419 We now apply the proposed velocity estimation method to a field GPR dataset acquired at the
420 Boise Hydrogeophysical Research Site (BHRS). The BHRS is a research wellfield located on
421 a gravel bar adjacent to the Boise River near Boise, Idaho, USA (Figure 6). The surficial aquifer
422 consists of late Quaternary fluvial deposits dominated by gravel and sand, and is underlain by
423 a layer of red clay at ~ 20 m depth (Barrash & Clemo 2002). The depth of the groundwater table
424 at the site varies seasonally between ~ 2 m and ~ 4 m. Over the past two decades, the BHRS has
425 been extensively utilized for the testing, validation, and improvement of a wide variety of
426 geophysical and hydrogeological characterization methods (e.g., Tronicke et al. 2004; Bradford
427 et al. 2009; Dafflon et al. 2009, 2011; Hochstetler et al. 2016; Xu et al. 2020, 2021).

428

429 The considered common-offset, bi-static GPR reflection profile is a part of 3D survey
430 performed at the BHRS in 1998 using a Pulse Ekko Pro 100 system (Sensors & Software Inc.)
431 with 100 MHz nominal center frequency antennas, and can be considered as a reference for
432 surface-based GPR reflection data collected in alluvial environments (e.g., Xu et al., 2020,
433 2021). The profile has a length of 30 m and crosses three boreholes, B5, A1, and B2, for which
434 neutron-neutron porosity logs are available below the groundwater table (Figure 6). While the
435 exact values have not been reported, the depth of the latter at the time of acquisition of the GPR
436 data and neutron-neutron logs was approximately 2 m. The GPR data were collected using a
437 constant antenna spacing of 1 m, a lateral trace increment of 0.1 m, and a time sampling interval
438 of 0.8 ns. For each recorded trace, 32 stacks were performed to improve the signal-to-noise

439 ratio. Antenna positioning errors and differences in antenna coupling across the profile were
440 estimated to be negligible. Figure 7 shows the GPR reflection section after minor pre-
441 processing.

442

443 3.2.2 Velocity estimation

444 The considered field GPR data were subjected to a processing flow consisting of, in order,
445 time-zero correction, DC shift removal, “de-wow” filtering, removal of the direct air and
446 ground arrivals, correction for the antenna offset, and amplitude scaling. Time-zero was
447 determined based on the first deflection of the data above the ambient noise level. While
448 slightly different approaches are possible, we estimate that the corresponding uncertainties do
449 not exceed ~ 2 ns. To correct for antenna offset, we used the average velocity of the vadose
450 zone of 0.14 m/ns inferred from previous work (e.g., Bradford, 2008; Bradford et al., 2009).
451 Contrary to our synthetic examples which involved an antenna spacing of 0.5 m, correction for
452 the larger offset between the antennas in the case of the BHRS data was deemed necessary and
453 should lead to negligible differences in traveltime beneath the direct air and ground arrivals
454 compared to the corresponding zero-offset acquisition. Due to the proximity of the direct
455 arrivals to the reflection from the groundwater table, we used a manual surgical mute to remove
456 them as opposed to the average trace subtraction technique considered previously. As was done
457 for the synthetic data, amplitude scaling was performed using a gain function of the form
458 $g(t) = (1 + at)e^{bt}$, where the parameters a and b that best balanced the amplitudes along
459 any given trace were found to be 0.5 ns^{-1} and 0.8 ns^{-1} , respectively. It is important to emphasize
460 that, with this choice of gain function that smoothly varies in time, the relative reflection

461 amplitudes along the GPR traces are importantly well preserved, which would not be the case
462 with the use of an AGC-type amplitude scaling.

463

464 Figure 8a shows the processed GPR section, to which we then applied the proposed velocity
465 estimation methodology. Following the workflow described in Section 2 and illustrated in
466 Figure 1, we began with the separation of the diffractions (Figure 8b) which, although not
467 evident in the original processed data, turn out to be quite abundant, particularly in the central
468 part of the profile. This was followed by the estimation of the RMS velocity structure (Figure
469 8c) and subsequent Dix inversion to infer the background velocity field (Figure 8d). The latter
470 points to the presence of a rather prominent low-velocity zone at intermediate depths in the
471 left-hand side of the profile. The inferred RMS velocity structure was then used to perform
472 time-migration of the GPR section (Figure 8e) which, overall, appears to result in an adequate
473 focusing and imaging of the data. An exception are the artefacts introduced into the uppermost
474 part of the section, which are likely related to the harsh surgical muting of the direct wave as
475 well as its potential interference with the neighboring reflection from the groundwater table.
476 Figure 8f shows the reflected wavefield that was extracted from the migrated section, which
477 we see to be largely devoid of these artefacts. After estimating the effective mixed-phase source
478 wavelet (Figure 8g) using the method of Schmelzbach and Huber (2015), we proceeded to
479 invert the imaged reflected wavefield for the underlying velocity perturbations using a value
480 of $\alpha = 10$, whose choice was based on the typical aspect ratio encountered in similar
481 heterogeneous environments as well as previous BHRS studies (Gelhar, 1993; Xu et al., 2020,
482 2021). The results, which are shown in Figure 8h, clearly depict the dramatic velocity

483 discontinuity associated with the groundwater table. Finally, Figures 8i and 8j show the
 484 superposition of the large-scale background velocity structure (Figure 8d) and the inverted
 485 small-scale velocity perturbation field (Figure 8h) in terms of two-way traveltimes and depth,
 486 respectively. Note that in deriving the latter, we also accounted for some mild topographic
 487 variations that were present along the profile. Note that, in the case of significant topographic
 488 variations, such variations would need to be corrected for earlier in our analysis procedure.

489

490 Although the inferred velocity distribution presented in Figure 8j is clearly dominated by the
 491 sharp transition from high to low velocities across the water table, the underlying saturated
 492 zone shows a significant degree of velocity heterogeneity. This heterogeneity largely emulates
 493 the structure depicted by the reflected wavefield in Figure 8d and, as such, is geologically
 494 plausible. To further assess the realism of our results, we compare them with the neutron-
 495 neutron porosity logs available in the saturated zone for boreholes B5, A1, and B2 (Figure 6).
 496 To this end, we transform the porosity logs to GPR velocity v using a standard petrophysical
 497 mixing model (e.g., Huisman et al. 2003)

$$v = \frac{c}{\sqrt{\varepsilon_r^s(1 - \phi) + \varepsilon_r^w \phi}}, \quad (19)$$

498 where $c = 0.3$ m/ns is the speed of light in free space, ϕ is the porosity, and $\varepsilon_r^s = 4.6$ and
 499 $\varepsilon_r^w = 80$ are the relative dielectric permittivities of the dry solid matrix and water, respectively.

500 A relative dielectric permittivity of 4.6 for the dry matrix corresponds to the average value for
 501 quartz (e.g., Schön, 2015) and, as such, is widely regarded as being suitable for alluvial
 502 environments in general and the BHRS in particular. Indeed, Dafflon et al. (2009) demonstrated
 503 the overall suitability of a relative dielectric permittivity of 4.6 for the solid matrix at the BHRS.

504 While variations in this parameter on the order of 10 to 15% are conceivable, the associated
505 uncertainties are minor and, hence, largely irrelevant compared to other sources of uncertainty
506 in our inversion results and the neutron-neutron logs.

507

508 Figure 9 shows the comparison between the GPR-derived velocity and the converted porosity
509 logs at the borehole locations. Overall, we see that the curves are in good agreement, not only
510 in terms of the trend, but also with regard to the absolute values. In this context, it is important
511 to note that the inferred velocity estimates are at least as accurate as those previously inferred
512 from multi-offset GPR reflection tomography (Bradford et al., 2009), while at the same time
513 exhibiting a significantly higher resolution. Arguably, the most conspicuous mismatch between
514 the GPR- and neutron-neutron-based velocity profiles is a seemingly systematic depth shift of
515 $\sim +0.5$ m of the former with regard to the latter, which was recently discussed by Xu et al.
516 (2021). This could be related to the depth calibration of the neutron-neutron logs and/or to a
517 systematic overestimation of the GPR velocity in the vadose zone, the latter of which is the
518 most poorly constrained part of our inferred velocity model due to partial interference between
519 the direct arrivals and the reflection from the water table. Conversely, this apparent mismatch
520 is unlikely to be related to the time-zero determination, whose uncertainty is estimated to be
521 on the order of 2 ns.

522

523 **4 Discussion and Conclusions**

524 We have presented in this paper a novel method for estimating the detailed high-frequency
525 electromagnetic velocity distribution in the shallow subsurface from surface-based common-

526 offset GPR reflection data. The smooth background component of the velocity structure is
527 estimated from the diffracted part of the recorded wavefield, whereas the superimposed small-
528 scale fluctuations are inferred from the associated reflected component. An important and
529 distinguishing feature of our methodology is that, in contrast to previous related approaches
530 (e.g., Schmelzbach et al. 2012; Liu et al. 2018; Xu et al. 2021), it does not require any borehole
531 calibration and/or conditioning information. It does, however, inherently rely upon the
532 presence of diffractions in the GPR data. In this regard, it is important to note that, although
533 diffractions are often not immediately obvious in a GPR profile, they can become much more
534 evident after wavefield separation. This is clearly illustrated in Figure 8.

535

536 The proposed technique was tested and validated on synthetic data corresponding to two
537 velocity models of differing complexity and realism: one an idealized layered model containing
538 a small number of discrete diffractors, and the other a stochastic facies-based model emulating
539 the typical heterogeneity observed in surficial alluvial environments (e.g., Gelhar 1993;
540 Tronicke et al. 2004; Tronicke and Holliger 2005). These synthetic tests not only illustrate the
541 fundamental validity and robustness of our method, but also allow us to identify a number of
542 features that merit attention during its application. Successful validation of our approach on the
543 BHRS field data further illustrates its capacity for estimating complex velocity structures.

544

545 Results for our synthetic test involving the stochastic subsurface model (Figures 4 and 5)
546 showed a loss of accuracy in the shallowest part of the inferred velocity distribution due to the
547 elimination of the direct air and ground arrivals, which removed important reflections from this

548 zone. Processing techniques used for this purpose, such as subtracting the average trace in a
549 corresponding time window, will thus affect the inferred velocity model over an initial depth
550 range of roughly 1-2 dominant wavelengths (Figures 4 and 5). Another interesting feature
551 emerging from the stochastic synthetic example is the fact that we fail to fully resolve the thin
552 low-velocity zone between ~ 2 m and ~ 3.5 m depth, notably in the central and right-hand side
553 of the profile. A bias in the estimated background velocity distribution over these depths
554 (Figure 5d) is likely the cause of this result. Given that this region has a density of diffractions
555 that is comparable to the rest of the model, this may point to the inherently limited resolution
556 of the inferred background velocity field. Under ideal circumstances, diffraction-based velocity
557 analysis can be expected to achieve a resolution on the order of one dominant wavelength,
558 which for the considered synthetic data is of the order of ~ 1 m. In practice, however, the
559 achievable resolution critically depends on the so-called smoothing radius parameter, which
560 controls the regularization of a number of steps in the diffraction velocity analysis procedure
561 (Fomel et al., 2007). As recently illustrated by Yuan et al. (2019), a smoothing radius that is
562 too small leads to unstable estimates of the diffraction-derived velocity model, whereas one
563 that is too large will lower unnecessarily its resolution. While we made every effort to
564 determine an optimal value of the smoothing radius for all data considered in this study, there
565 may be regions in the final velocity model where the large- and small-scale components
566 inadequately complement each other due to the limited resolution of the former.

567

568 Arguably, the most important criterion that must be fulfilled for our method to perform
569 satisfactorily is the presence of an ample amount evenly distributed diffractions throughout the

570 recorded constant-offset GPR section. Given the inherent heterogeneity of the shallow
571 subsurface (e.g., Gelhar, 1993; Hubbard and Rubin, 2005; Dafflon et al., 2009; Xu et al., 2021),
572 this condition is likely to be fulfilled even if the diffracted energy is not directly obvious in the
573 original recorded data (Figures 5 and 8). Nonetheless, in the case where an sufficient amount
574 of diffracted energy cannot be retrieved through wavefield separation and/or where the
575 diffraction events are highly unevenly distributed throughout the probed subsurface region,
576 standard common-midpoint-type analyses may still be used to estimate the large-scale velocity
577 structure with our methodology. Under these circumstances, only the estimation of the
578 background field would change, and the inversion for the small-scale velocity fluctuations
579 would remain the same.

580

581 Two final assumptions upon which our method relies are that the recorded GPR wavefield is
582 largely non-dispersive and is dominated by single scattering. This allows us to use a
583 convolutional model to describe the reflection data, which in turn permits us to pose the
584 velocity perturbation estimation procedure as a highly efficient linear inverse problem. Limited
585 signal attenuation, and thus limited dispersion, is a prerequisite for acquiring surface-based
586 common-offset GPR reflection data of adequate quality and depth of penetration. The practical
587 validity of this assumption is notably underscored by the success of numerous studies explicitly
588 relying upon an adequate estimation of the GPR source wavelet (e.g., Schmelzbach et al., 2012;
589 Schmelzbach and Huber, 2015; Liu et al., 2018; Xu et al., 2021). While it is theoretically
590 conceivable that there exist environments where multiple scattering becomes sufficiently
591 important in GPR studies, the results of extensive testing of the convolutional model on

592 synthetic and field data suggest that the effects of multiples are largely negligible in near-
593 surface environments (e.g., Irving et al., 2009; Schmelzbach et al., 2012; Xu et al., 2020,2021).
594 Indeed, in such environments, the combination of small reflection coefficients and signal
595 attenuation due to conductivity-related losses means that multiply reflected energy is not strong.
596 The latter is consistent with a methodological study involving acoustic waves in strongly
597 heterogeneous environments, where it was found that multiple scattering only becomes
598 important for strong local velocity fluctuations, corresponding to standard deviations of the
599 order of 10% and more, in combination with long propagation paths in excess of ~ 20 dominant
600 wavelengths (e.g., Holliger, 1997). These conditions are generally not fulfilled for surface-
601 based constant-offset GPR reflection data.

602

603 An important characteristic of this work is that the proposed methodology is rather
604 straightforward. After basic processing of the GPR data in MATLAB, wavefield separation,
605 diffraction velocity analysis, and Dix inversion are carried out using the Madagascar software
606 package, which is well-established for this purpose. The subsequent wavelet estimation and
607 L1-norm inversion are then again performed in MATLAB. For all of the datasets considered in
608 this study, the total time required to complete all of the steps in our workflow is on the order
609 of one day. The IRLS inversion procedure itself proved to be stable and to converge to
610 consistent estimates of the velocity perturbation field after approximately five iterations. In
611 practical terms, the latter amounted to less than one minute of CPU time on a modest laptop
612 computer. Finally, the inherent computational efficiency of the convolutional model used in
613 our approach implies that the extension of the proposed method to 3D is conceptually

614 straightforward. The only challenge that we anticipate in this regard is the still somewhat
615 limited practical maturity of 3D diffraction velocity analysis techniques (e.g., Merzlikin et al.
616 2017; Bauer et al., 2020). A direct benefit of 3D analysis is that errors introduced into the
617 background velocity estimation procedure by out-of-plane diffractions can be avoided.

618

619 **Acknowledgements**

620 Yu Liu gratefully acknowledges financial support of this work through the China Scholarship
621 Council (CSC grant number 201806320359). The considered GPR field data were collected by
622 Michael Knoll and Warren Barrash as part of the initial BHRS characterization, and were
623 kindly provided to us by John Bradford together with the corresponding neutron-neutron
624 porosity logs.

625

626 **Data availability**

627 The data underlying this article will be shared on reasonable request to the corresponding
628 author.

629

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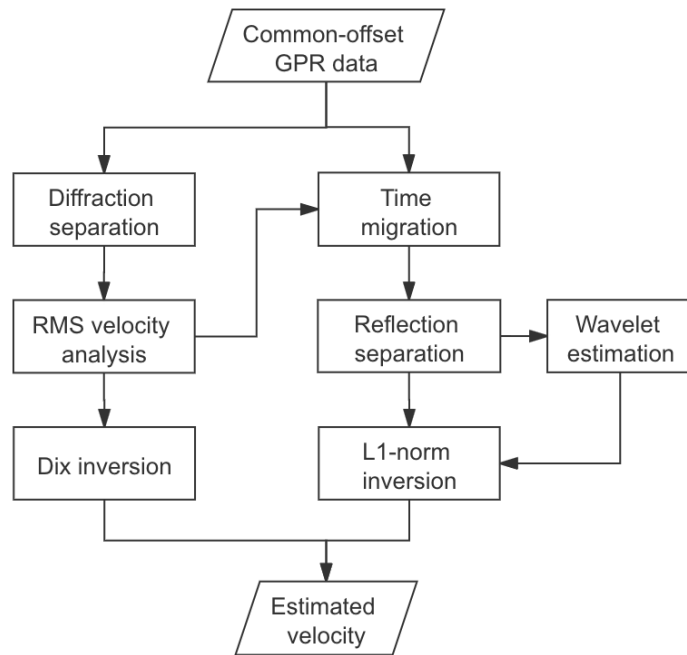


Figure 1. Flowchart illustrating the proposed method for estimating the detailed subsurface velocity structure from surface-based common-offset GPR reflection data.

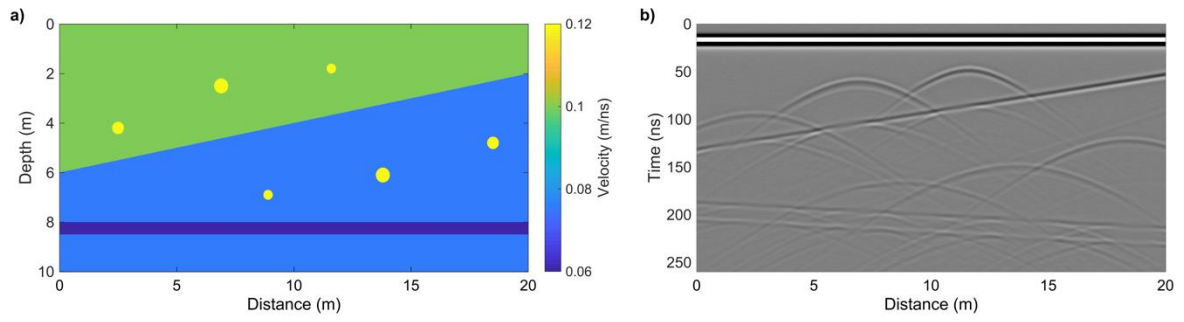


Figure 2. a) Layered model velocity with discrete diffractors and b) corresponding synthetic common-offset GPR reflection data with 2% Gaussian random noise added.

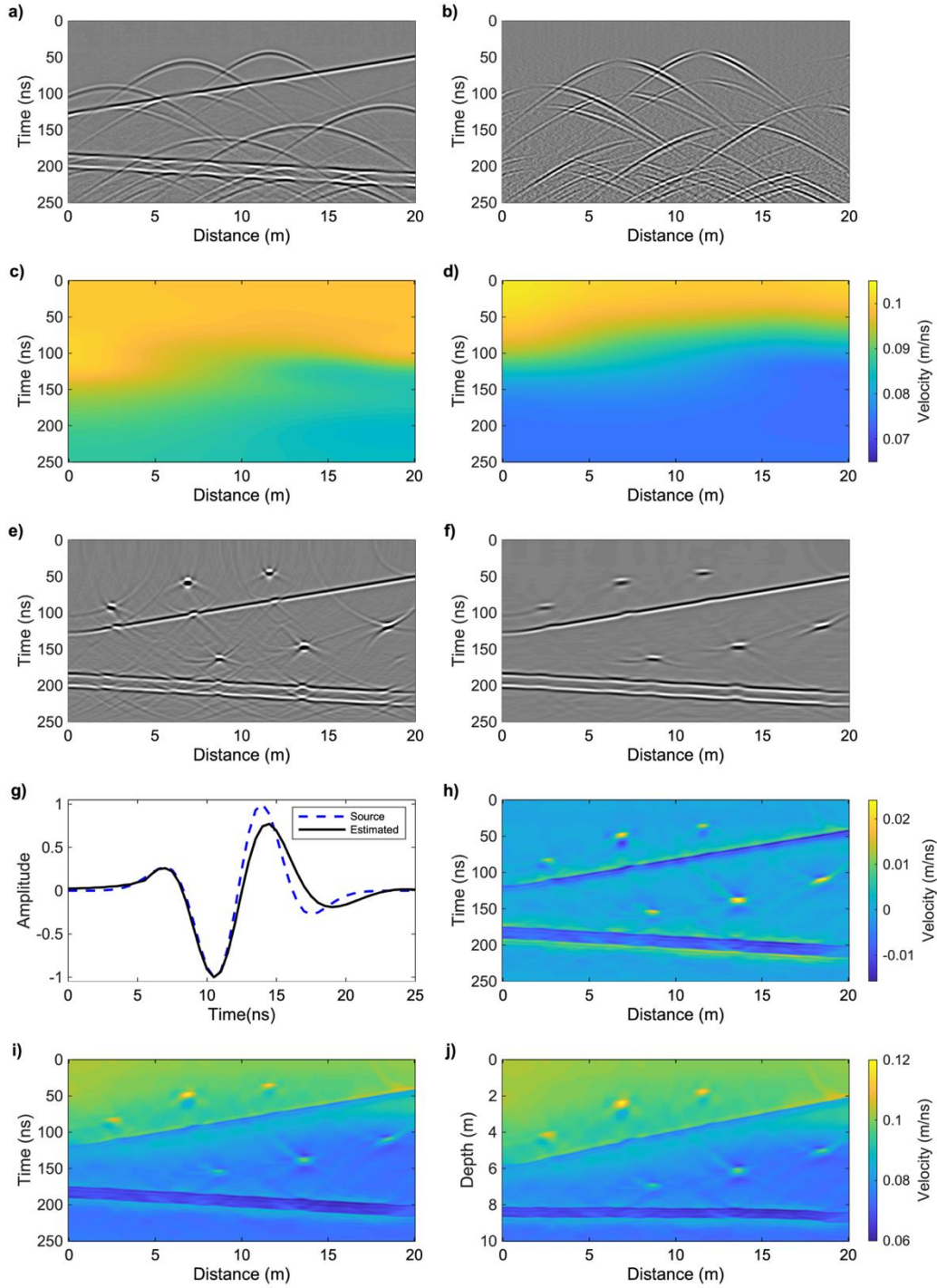


Figure 3. Velocity estimation process for the layered synthetic velocity model presented in Figure 2a. From the **a)** processed GPR section, the **b)** diffracted wavefield is separated and used to estimate the **c)** RMS velocity structure. Using Dix inversion, the **d)** low-frequency background velocity field $v_0(x, t)$ is obtained. **e)** Time-migrated GPR section based on the RMS velocity structure, from which the **f)** reflected wavefield is obtained. **g)** Comparison of estimated GPR wavelet with the true source wavelet. **h)** Velocity perturbation field $\Delta v(x, t)$ obtained by inverting the reflected wavefield. The final estimated velocity structure (background+perturbation) is shown in terms of **i)** traveltim and **j)** depth.

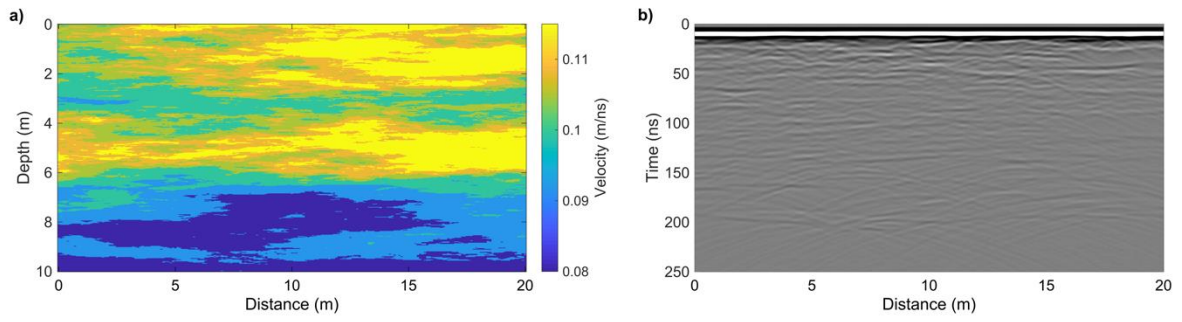


Figure 4. a) Stochastic velocity model and b) corresponding synthetic common-offset GPR reflection data with 2% Gaussian random noise added.

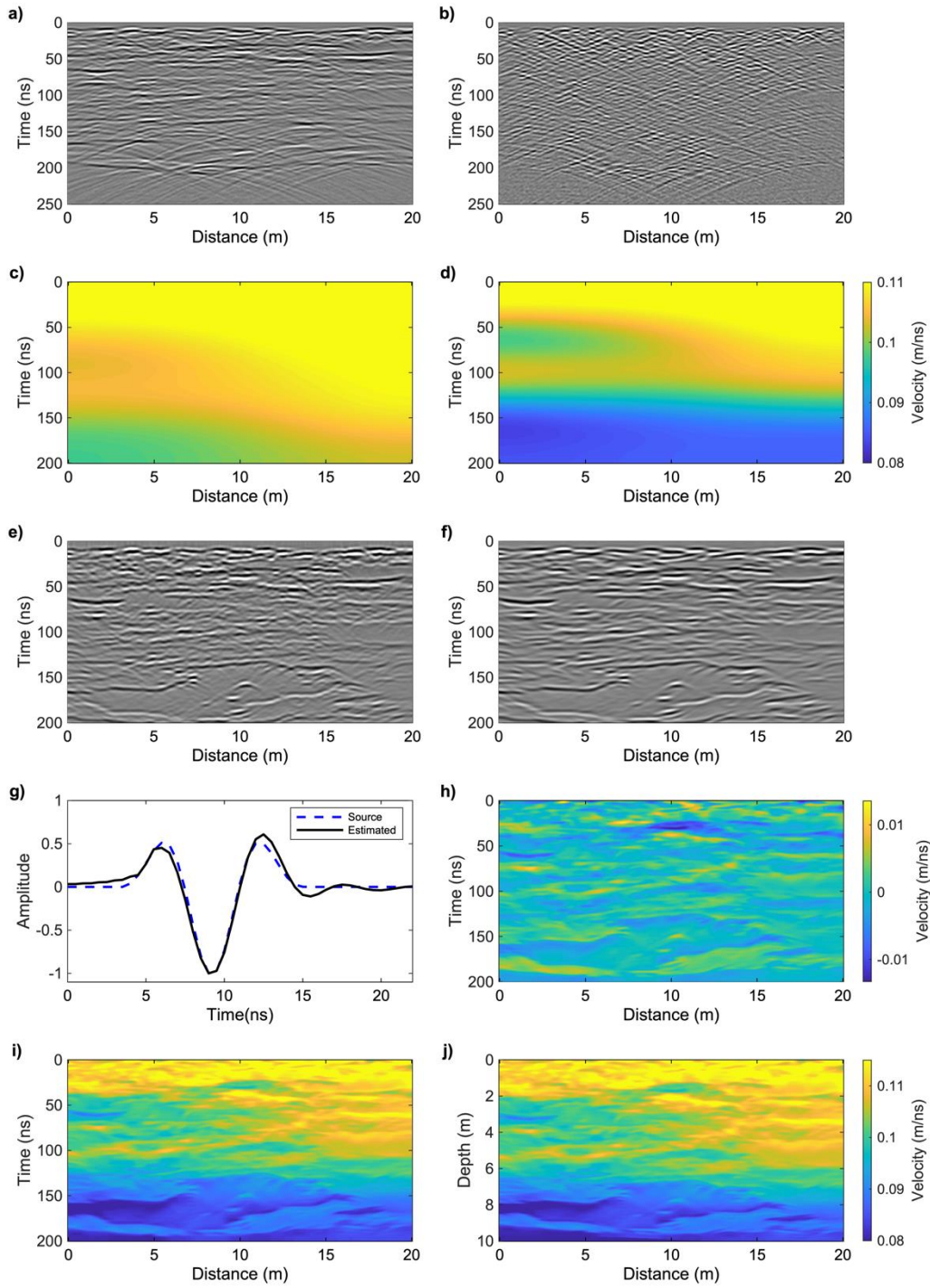


Figure 5. Velocity estimation process for the stochastic synthetic velocity model presented in Figure 4a. From the **a)** processed GPR section, the **b)** diffracted wavefield is separated and used to estimate the **c)** RMS velocity structure. Using Dix inversion, the **d)** low-frequency background velocity field $v_0(x, t)$ is obtained. **e)** Time-migrated GPR section based on the RMS velocity structure, from which the **f)** reflected wavefield is obtained. **g)** Comparison of estimated GPR wavelet with the true source wavelet. **h)** Velocity perturbation field $\Delta v(x, t)$ obtained by inverting the reflected wavefield. The final estimated velocity structure (background+perturbation) is shown in terms of **i)** traveltime and **j)** depth.

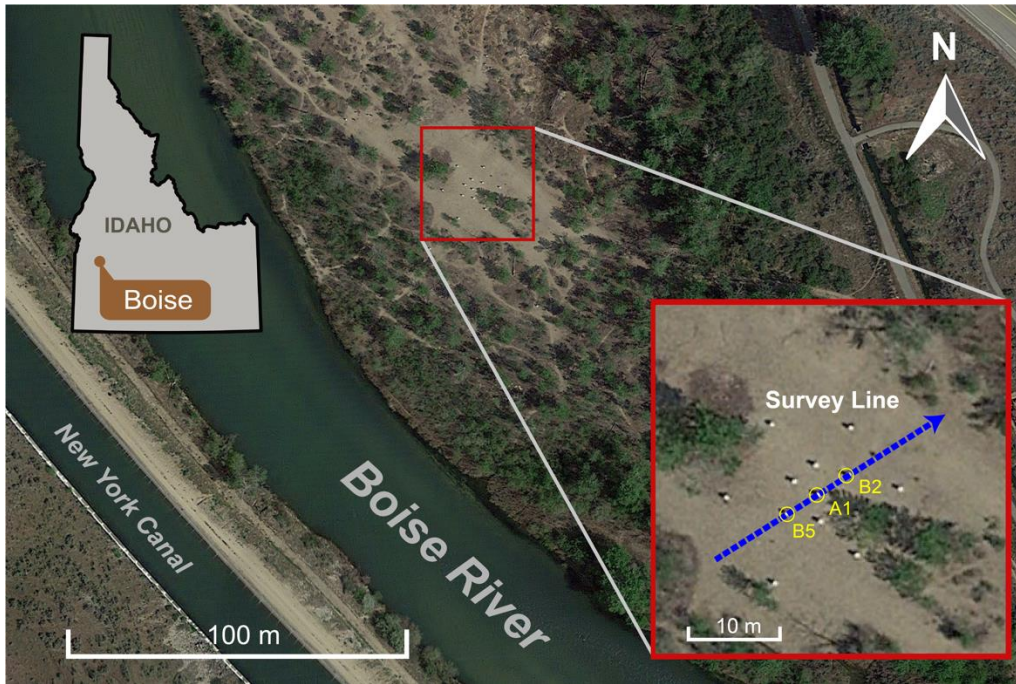


Figure 6. Map of the BHRS showing the location of considered common-offset GPR reflection profile (blue dashed line). The profile is aligned with boreholes B5, A1, and B2 (yellow circles).

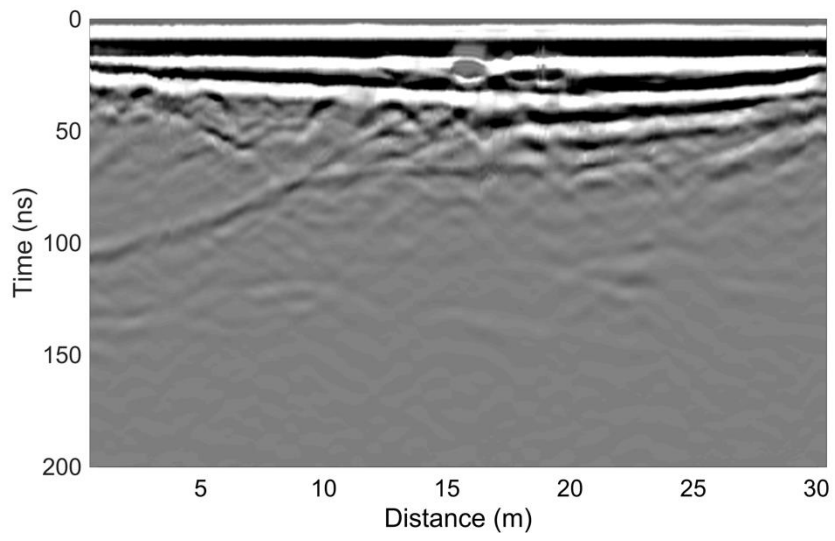


Figure 7. Common-offset GPR reflection section from the BHRS after minor preprocessing consisting of time-zero correction and “de-wow” filtering.

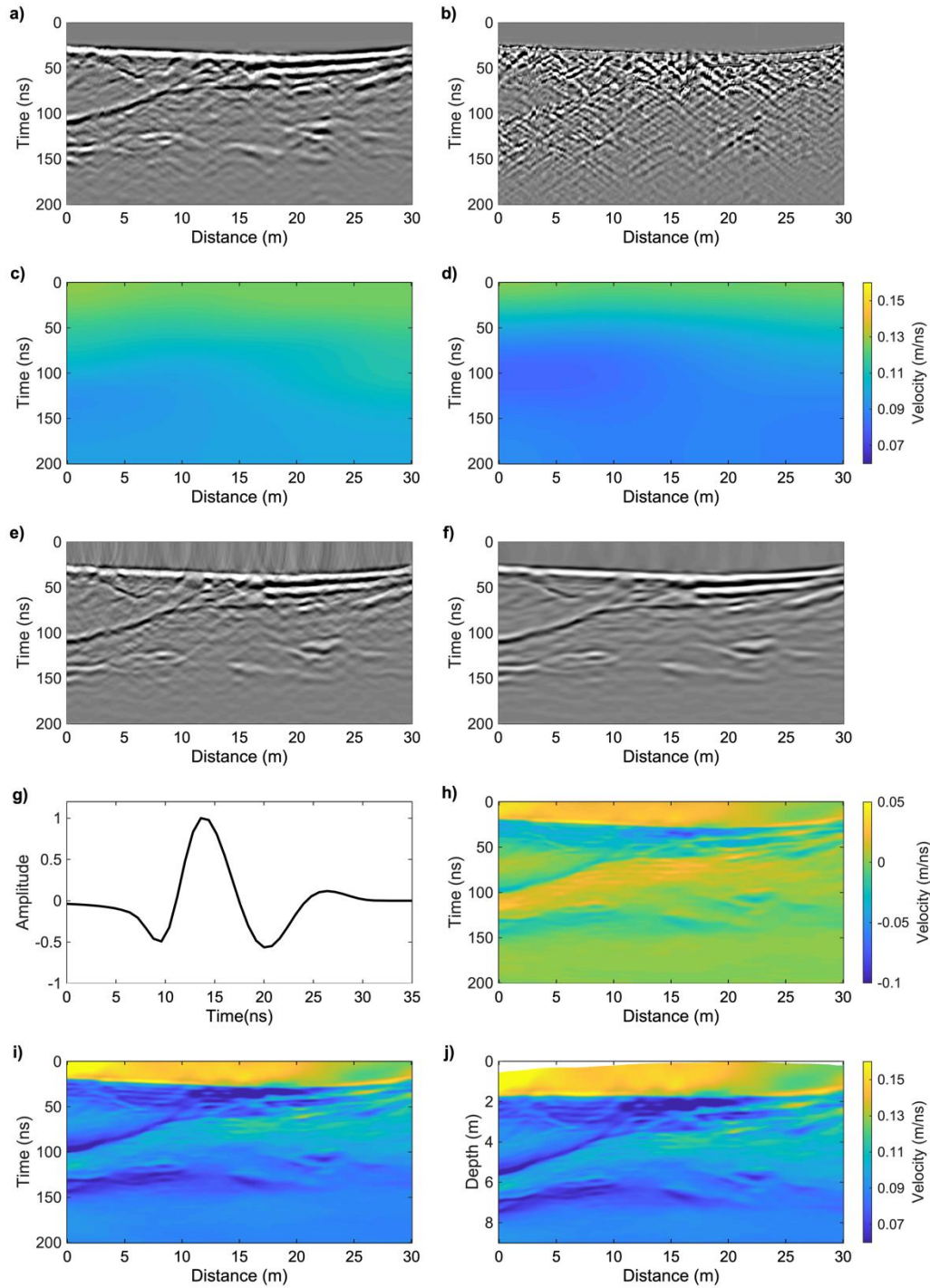


Figure 8. Velocity estimation process for the BHRS field data presented in Figure 7. From the **a)** processed GPR section, the **b)** diffracted wavefield is separated and used to estimate the **c)** RMS velocity structure. Using Dix inversion, the **d)** low-frequency background velocity field $v_0(x, t)$ is obtained. **e)** Time-migrated GPR section based on the RMS velocity structure, from which the **f)** reflected wavefield is obtained. **g)** Estimated GPR source wavelet. **h)** Velocity perturbation field $\Delta v(x, t)$ obtained by inverting the reflected wavefield. The final estimated velocity structure (background+perturbation) is shown in terms of **i)** traveltimes and **j)** depth.

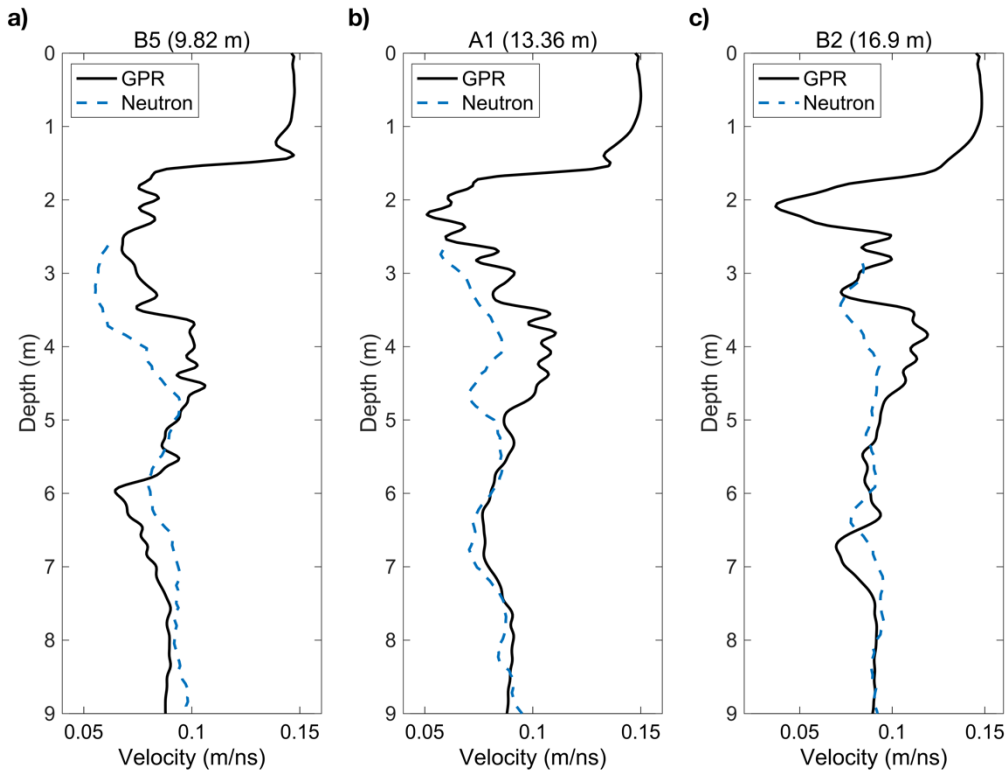


Figure 9. Comparison of the velocity estimated from the common-offset GPR reflection data from the BHRS along boreholes **a)** B5, **b)** A1 and **c)** B2 (black solid lines) with the corresponding converted neutron-neutron porosity logs (blue dashed lines).